Corrigenda

G. HETSRONI, E. WACHOLDER, and S. HABER, "Heat Conduction in Reactor Fuel Elements," *Nucl. Sci. Eng.*, **37**, 329 (1969).

A number of typographical errors appear in the article. The corrected equations should read:

$$\xi_n \equiv -\left[\frac{2k_1}{(k_2 - k_1)\sinh(2\lambda_n X_0)} + \operatorname{cotanh}(\lambda_n X_0)\right] \quad . \tag{20}$$

$$f_0(r) = \hat{B}_0 - \frac{q_0''' r^2}{2\pi k_1} \quad . \tag{35a}$$

$$\hat{\beta}_0 = -\frac{q_0''' X_0^2}{k_2 \pi} \tag{37a}$$

$$(\hat{B}_n - \hat{\beta}_n)\, I_0(\lambda_n X_0) - \hat{\alpha}_n K_0(\lambda_n X_0) = -K_n \tag{38a}$$

$$\left(\frac{k_1}{k_2}\hat{B}_n - \hat{\beta}_n\right) I_1(\lambda_n X_0) + \hat{\alpha}_n K_1(\lambda_n X_0) = 0 \quad , \tag{38b}$$

$$\hat{\beta}_n = \frac{k_2}{k_2 - k_1}\hat{\alpha}_n\left[\frac{k_1}{k_2}\frac{K_0(\lambda_n X_0)}{I_0(\lambda_n X_0)} + \frac{K_1(\lambda_n X_0)}{I_1(\lambda_n X_0)}\right] - \frac{k_1}{k_2 - k_1} \times \frac{K_n}{I_0(\lambda_n X_0)} \tag{39}$$

$$\hat{B}_n = \frac{k_2}{k_2 - k_1}\hat{\alpha}_n\left[\frac{K_0(\lambda_n X_0)}{I_0(\lambda_n X_0)} + \frac{K_1(\lambda_n X_0)}{I_1(\lambda_n X_0)}\right] - \frac{k_2}{k_2 - k_1} \times \frac{K_n}{I_0(\lambda_n X_0)} \quad . \tag{40}$$

$$B_0 = -\hat{\beta}_0\left[\frac{k_2}{X_1 h} + \ln\frac{X_1}{X_0} - \frac{WL}{2X_1}\right] + \frac{2}{\pi}\sum_{n=1}^{\infty}\frac{1}{n}\left[\hat{\beta}_n I_1(\lambda_n X_1) - \hat{\alpha}_n K_1(\lambda_n X_1)\right] + \frac{q_0''' X_0^2}{2\pi k_1} \qquad n\text{ - odd} \tag{41}$$

while α_n is obtained from the matrix equation

$$\hat{J}_{nj} = -W a_{jn}\left\{\frac{k_2}{k_2 - k_1}\left[\frac{k_1}{k_2}\frac{K_0(\lambda_j X_0)}{I_0(\lambda_j X_0)} + \frac{K_1(\lambda_j X_0)}{I_1(\lambda_j X_0)}\right] \times I_1(\lambda_j X_1) - K_1(\lambda_j X_1)\right\} \tag{43}$$

$$\hat{D}_{nn} = \left[\frac{k_2}{h}\lambda_n K_1(\lambda_n X_1) - K_0(\lambda_n X_1)\right] + \left[\frac{k_2}{h}\lambda_n I_1(\lambda_n X_1) + I_0(\lambda_n X_1)\right]\left[\frac{k_1}{k_2 - k_1}\frac{K_0(\lambda_n X_0)}{I_0(\lambda_n X_0)} + \frac{k_2}{k_2 - k_1} \times \frac{K_1(\lambda_n X_0)}{I_1(\lambda_n X_0)}\right] \tag{44}$$

$$\hat{P}_n = -\frac{4W\hat{\beta}_0}{\lambda_n^2 L X_1} \tag{46}$$

$$B_0 = -\alpha_0\left[\frac{k_2}{h} + X_1 - \frac{WL}{2}\right] + \frac{2q_0''' X_0^2}{\pi}\left(\frac{1}{2k_1} - \frac{1}{k_2}\right) + W\sum_{n=1}^{\infty}\frac{4\alpha_n}{n\pi}\left[\cosh(\lambda_n X_1) + \xi_n \sinh(\lambda_n X_1)\right] \qquad n\text{ - odd} \quad . \tag{A-6}$$

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A. GANDINI, "A Method of Correlation of Burnup Measurements for Physics Prediction of Fast Power Reactor Life," *Nucl. Sci. Eng.*, **38**, 1 (1969).

Dr. G. Cecchini has pointed out that Eq. (35) on p. 4 is generally valid when $\delta\mathcal{B}$ is proportional to $\mathcal{B}$, i.e., $\delta\mathcal{B} = \alpha\mathcal{B}$, where α has an arbitrary value. Otherwise, Eq. (25) should be used. This limitation does not seem to affect, however, the applicability of these methods to the correlation of the irradiation integral data, provided first-order terms are sufficient for an accurate treatment.